

APPLICATION
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TITLE: BIOCOMPATIBLE ARTICLE
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Biocompatibl articl

The invention relates to an, in particular
5 biocompatible, article, in particular an implant such
as a stent, to a process for its production and to its
use.

Modern biomedical science is distinguished by
bringing natural organic fluids and tissues into
10 contact with synthetic articles in order to imitate or
influence defined physiological processes. Examples
include the insertion of implants, extracorporeally
used medical appliances or the *in vitro* cultivation of
particular cell cultures in an artificial environment.

15 The principle applying in these cases is that
greater compatibility between the natural and the
synthetic substances leads to a better result. Bio-
compatibility thus relates to the specific use of a
technically defined material in a physiologically
20 defined environment with the aim of assisting or
replacing specific physiological functions. Thus, for
example, the surface for an orthopedic prosthesis would
ideally be designed so that it is able to become
incorporated in the bone as quickly as possible, but at
25 the same time the risk of infection should be low. The
biological compatibility of a stent for coronary
arteries would be optimal if its thrombogenicity is
only slight or absent and there is minimal or
absolutely no influence on the function of the cells in
30 the direct vicinity, for example the endothelial cells;
in particular, proliferation of cells of the so-called
intimal layer of the vessel wall should be avoided.

Another success of modern medicine is the
temporary replacement of organs or their functions by
35 medical appliances, for example hemodialysis, cardiac
bypass or extracorporeal membrane oxygenation (ECMO).
In these cases too there is a direct relation between
biocompatibility and the incidence of complications,
some of which are life-threatening, such as hemolysis

or hemorrhagic complications as a result of iatrogenic anticoagulation induction.

In the past there have been many approaches to solving the problems described, at least in part. Thus,
5 the research group of Dunn et al. attempted in 1994 (Ciprofloxacin Attachment to Porous-Coated Titanium Surfaces, D.S. Dunn, S. Raghavan, R.G. Volz, Journal of Applied Biomaterials, Vol. 5, 325-331, 1994) to modify a titanium surface in order to deposit the antibiotic
10 ciprofloxacin thereon.

Constrictions in the coronary vessels of the heart in particular are nowadays treated to an increasing extent by the implantation of stents. These stents consist of medical stainless steel, tantalum,
15 Nitinol or titanium (see DE-A-195 33 682, DE-A-196 53 708, Characteristics of metals used in implants, I. Gotman, J. Endourol., 11(6):383-389; and US-A-5,356,433). However, two serious complications may occur when they are used. On the one hand, blood coagulation is activated by the metal. This may lead to blockage of the stent by a thrombosis especially within the first four days after implantation. The second problem on use of coronary stents is restenosis due to intimal hyperplasia. The coronary vessel of the heart
20 is composed of three layers of tissue, the intima, media and adventitia. The intima consists of endothelial cells which line the lumen of the vessel and are in direct contact with the bloodstream. The boundary between it and the media, which consists of
25 smooth muscle cells, is formed by the so-called internal elastic lamina. The outer layer, adventitia, then forms the connection between the vessel and surrounding tissue. Histological investigations show that introduction of stents leads to a lesion of the
30 endothelial layer of the intima and, in particular, of the internal elastic lamina. The body reacts to this irritation with a proliferation of intimal cells, which is called intimal hyperplasia, which may be so exten-

sive that renewed blockage of the lumen of the vessel takes place inside the stent.

Technical attempts have been made to reduce the tendency to thrombosis and/or intimal hyperplasia by various coatings on stents. Thus, EP-A-0 836 839 discloses a gold layer on a stent. Antithrombogenic Coating of Stents Using a Biodegradable Drug Delivery Technology, R. Herrmann, G. Schmidmaier, B. Märkl, A. Resch, I. Hähnel, A. Stemberger, E. Alt; Thromb. Haemost., 82, 51-57, 1999 discloses stents with steel or gold surfaces coated with biodegradable polylactic acid. The article "Local drug delivery of argatroban from a polymeric-metallic composite stent reduces platelet deposition in a swine coronary model", K.R. Kruse, J.J. Crowley, J.F. Tanguay, R.M. Santos, D.S. Millare, H.R. Phillips, J.P. Zidar, R.S. Stack, Catheter Cardiovasc. Interv., 46(4), 503-7, 1999 relates to a polymer-metal stent which is provided with argatroban. The antiproliferative agent Taxol and the antiinflammatory substance dexamethasone have, besides the anticoagulant medicament heparin (DE-A-195 33 682), been applied to stents, cf. Antiproliferative stent coatings: Taxol and related compounds, C. Herdeg, M. Oberhoff, K.R. Karsch, Semin. Interv. Cardiol., 3, 25 (3-4), 179-9, 1998; and Anti-inflammatory Stent Coatings. Dexamethasone and Relates Compounds, S.H. Park, A.M. Lincoff, Semin. Interv. Cardiol., 3(3-4):191-5, 1998. A stent provided with a coating of silicon carbide has also been investigated in clinical studies on the reduction of endothelial proliferation and platelet activation, cf. Silicon carbide-coated stents: clinical experience in coronary lesions with increased thrombotic risk, B. Heublein, C. Ozbek, K. Pethig, J. Endovasc. Surg., 5(1), 32-6, 1998; and Silicon-carbide coated coronary stents have low platelet and leukocyte adhesion during platelet activation, S.H. Monnink, A.J. van Boven, H.O. Peels, I. Tigchelaar, P.J. deKam, H.J. Crijns, W. van Oeveren, J. Investig. Med., 47(6), 304-10, 1999.

Coated stents are also described in Coated stents: local pharmacology, V.K. Raman, E.R. Edelman, Semin. Interv. Cardiol., 3(3-4), 133-7, 1998; In vivo evaluation of a fluorine-acryl-styrene-urethane-silicone antithrombogenic coating material copolymer for intravascular stents, T. Matsuhashi, H. Miyachi, T. Ishibashi, K. Sakamoto, A. Yamadera, Acad. Radiol., 3(7), 581-8, 1996; and Antithrombogenic coating of stents using a biodegradable drug delivery technology, R. Herrmann, G. Schmidmaier, B. Markl, A. Resch, I. Hahnel, A. Stemberger, E. Alt, Thromb. Haemost., 82(1), 51-7, 1999.

Besides these approaches, attempts have also been made to cover surfaces with covalently modified albumin, cf. The Potent Platelet Inhibitory Effects of S-Nitrosated Albumin Coating of Artificial Surfaces, N. Maalej, R. Albrecht, J. Loscalzo, J.D. Folts, J.A.C.C., 33(5), 1408-1414, 1999; and Adherence and Proliferation of Endothelial Cells on Surface-Immobilized Albumin-Heparin Conjugate, G.W. Bos, N.M. Scharenborg, A.A. Poot, G.H.M. Engbers, J.G.A. Terlingen, T. Beugeling, W.G. Van Aken, J. Feijen, Tissue Engineering, 4(3), 267-279, 1998. In Hydration and preferential molecular adsorption on titanium *in vitro*, K.E. Healy and P. Bucheyne, Biomaterials 1992, Vol. 13, No. 8, 553-561, the behavior of titanium towards human serum was investigated by surface spectroscopy.

None of the developed methods has yet led to a convincing product on the market. Whereas the occurrence of stent thromboses can at present be treated sufficiently well by systemically administered medicaments, called platelet aggregation inhibitors, there is as yet no satisfactory therapy for restenosis due to intimal hyperplasia.

The problems described above are solved according to the invention by an article comprising a substrate which is coated at least partly with at least one layer, and on which there is at least partly a

protein-, peptide- and/or saccharide-containing substance, where the layer directly adjacent to the substance comprises at least one metal selected from titanium, zirconium and hafnium, or a compound thereof with one or more nonmetals and/or semiconductors, or an alloy thereof with one or more other metals, and has been applied by means of a vacuum coating process. The invention additionally relates to a process for producing the article, in which a substrate is at least partly coated with at least one layer, and subsequently a protein-, peptide- and/or saccharide-containing substance is applied at least partly to the coated substrate, where the layer directly adjacent to the substance is applied using at least one metal selected from titanium, zirconium and hafnium, or a compound thereof with one or more nonmetals and/or semiconductors, or an alloy thereof with one or more other metals at a temperature of from 20 to 500°C under vacuum. The invention moreover relates to the use of the article for implantation, insertion or attachment in or on the animal or human body or for bringing into contact with animal or human blood or tissue or animal or human cells. The invention further comprises the use of a protein-, peptide- and/or saccharide-containing substance for application to a layer as defined above. Preferred embodiments of the invention are described in the following description, the figures, the examples and the dependent claims.

In the figures,

30 Fig.1 shows a diagrammatic representation of a preferred article according to the invention;

Fig.2 shows a graphical depiction of the results obtained in Example 1 described hereinafter; and

35 Fig.3 shows a graphical depiction of the results obtained in Example 2 described hereinafter.

An article is intended to mean for the purpose of the invention every appliance or every device which comes into contact, even for a short time, with human

or animal blood or tissue or with human or animal cells, or can be implanted into the human or animal body or inserted or attached for a longer or shorter period. Examples which may be mentioned are: catheters,
5 tubes, sensors, stents, artificial heart valves, endotracheal tubes or cardiac pacemakers.

The metal in the layer is preferably titanium. Besides this, a compound or alloy of titanium is also preferred. Preferred compounds, in particular ceramic
10 compounds, have the formula MC_xNyO_z , where M = Ti, Zr and/or Hf; x, y, z = 0 to 2.1; $x+y+z$ = 0.01 to 4, in particular $x+y+z$ = 0.01 to 2, particularly preferably $x+y+z$ = 0.05 to 1.5. Moreover the ratio of metal to nitrogen to oxygen to carbon is 1:(0 to 2.1):(0 to
15 2.1):(0 to 2.1), preferably 1:(0 to 1.0):(0 to 2.0):(0 to 1.0), particularly preferably 1:(0 to 0.8):(0 to 1.5):(0 to 0.3). The above ratios refer to the number
of particles or molar ratios. M is preferably titanium or a zirconium/titanium alloy. Besides titanium, zir-
20 conium and/or hafnium, the layer may also contain as additional metals niobium, tantalum, tungsten, molybdenum or alloys thereof, which has advantageous effects for the resistance of the layer to corrosion. Such alloys may furthermore have beneficial mechanical
25 properties. Preferred alloys are a titanium/aluminum/vanadium alloy, titanium/aluminum/niobium alloy, titanium/aluminum/iron alloy and a titanium/niobium/zirconium alloy. It is also possible for the layer to contain hydrogen (dissolved or preferably bound). Suitable as material for the layer are also materials like those described in DE-C-4 3 44 258 and DE-A-196 06 188. It is also possible to use a layer system in which a TiN layer, which is preferably about
30 0.5 μm thick, is applied to an electrically conducting intermediate layer of titanium suboxide, in particular of the composition $\text{TiO}_{1.7}$. This layer system is particularly corrosion-resistant.

The thickness of the layer is preferably in the range between 0 and 5 μm , more preferably from 50 to

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3000 nm, very preferably from 100 to 1000 nm. Such a layer thickness ensures that flexing of the particular article can also be tolerated without damage.

The layer preferably has a specific resistance
5 in the range from 10 to $10^7 \mu\Omega\text{cm}$, preferably from 50 to 100,000 $\mu\Omega\text{cm}$, particularly preferably from 50 to 10,000 $\mu\Omega\text{cm}$. The specific resistance can easily be adjusted by the skilled person by altering the content of oxygen, nitrogen and/or carbon within the scope of
10 experiments customary in the art. Measurements have shown that blood platelet adhesion has a maximum at 1000-10,000 $\mu\Omega\text{cm}$. The article can be adapted to the electrophysiological conditions by altering the electrical conductivity. The article can be adapted to the
15 physicochemical conditions by supplementing the layer with the protein-, peptide- and/or saccharide-containing substances provided according to the invention, which are also assisted where appropriate by agents with an antibiotic or pharmacological action.

20 The layer is present as a thin layer on a substrate. Suitable substrates are made of a metal such as molybdenum, silver, gold, copper, aluminum, tungsten, nickel, chromium, zirconium, titanium, hafnium, tantalum, niobium, vanadium, iron or mixtures or alloys
25 thereof, in particular stainless steel or Nitinol, or of a polymer such as polyester, polyamide, polyurethane (PU), polyethylene (PE), polytetrafluoroethylene (PTFE) or DACRON®. The substrate preferably consists of stainless steel, in particular medical stainless steel,
30 tantalum, Nitinol, titanium, gold or polymer. The layer is preferably applied to a rough substrate surface whose roughness is characterized by a random distribution of the deviations from the average level, and the standard deviation of this distribution is in
35 the range 0.5-50,000 nm, preferably 40-1200 nm. The substrate is at least partly, preferably completely, coated with the layer.

A layer which is directly adjacent to the substance and has been applied by a vacuum coating

process is also intended to mean for the purpose of the invention a layer which, after its application by a vacuum coating process, has been subjected to a natural aging process by breaking the vacuum, preferably in air or storage under normal conditions.

In a preferred embodiment, an intermediate layer is provided between substrate and layer, which has a greater adhesive strength. This intermediate layer consists of a metal, preferably of chromium, copper, nickel, molybdenum, tantalum, niobium, silver or alloys of these metals or a semiconductor, for example silicon.

Suitable protein-, peptide- and saccharide-containing substances are albumin; fibrinogen; heparins; collagen; blood proteins, for example alpha-2 globulin; immunoglobulins such as IgG, IgM, IgE IgA and proteins of the complement system, cytokines, interleukins and interferons; glycoproteins such as ferritin and lactoferrin; salivary proteins such as lysozyme, IgA2, mucin and glandulin; and/or alpha-1 proteinase inhibitors. These substances may be present either alone or in a mixture thereof. The preferred substances are albumin, fibrinogen, heparin or a mixture thereof. Albumin is most preferred, especially a mixture of albumin with fibrinogen, heparin and/or one or more of the other abovementioned substances, in particular albumin with fibrinogen. Albumin is a protein which is very soluble in water, is highly hydrated, is difficult to salt out, has an elliptical shape and a molecular weight of about 660,000, and has a content of sulfur-containing amino acids, an isoelectric point of 4.6 and amphotytic behavior. Particularly suitable albumins are human albumin, bovine albumin, pig albumin, chicken albumin, dog albumin, or albumin from cats, monkeys, guinea pigs, mice, turkeys, hamsters, rhesus monkeys or sheep. Human albumin is most preferred.

The substance is present on the layer at least in part, preferably completely.

The article according to the invention reduces foreign-body reactions and allows a wide variety of desired properties to be generated. Thus, for example, the restenosis rate is reduced to 53% by combining 5 albumin, preferably human albumin, with a TiN_xO_y layer on a stent substrate of medical stainless steel, where x and y are as defined above (cf. Example 3 herein-after). Other proteins, such as fibrinogen, reduce the adhesion of certain bacterial strains (cf. Example 2 10 hereinafter). This is particularly relevant for example to various catheters in the region of urogenital tract or blood system or to implants in the region of the respiratory tract.

To produce the article, the layer is applied by 15 a vacuum coating process to the substrate. This expediently takes place by PVD (*physical vapor deposition*), CVD (*chemical vapor deposition*), PECVD (*plasma enhanced chemical vapor deposition*) or ion plating, in particular by PVD processes such as 20 reactive vapor deposition, sputtering, reactive plasma processes or the process described in DE-A-195 06 188. Particularly suitable for applying the layer to the substrate is the following process: the substrate is positioned in a vacuum chamber and heated to 20 to 25 500°C, preferably to 100 to 400°C, particularly preferably 200 to 350°C. For the coating, the metal or the alloy as defined above is vaporized in the chamber via vaporization, preferably electron beam vaporization, under a vacuum of from 10^{-5} to 10^{-2} mbar, preferably 30 from 10^{-4} to 10^{-2} mbar, particularly preferably from 10^{-4} to 5×10^{-3} mbar. If compounds are to be applied, the corresponding gases, oxygen, nitrogen and/or carbon-containing gases such as, for example, ethyne or carbon dioxide, are introduced into the vacuum chamber. The 35 procedure in this case for generating the required chemical composition of the compound is preferably as follows:

The chemical composition is generally determined by the parameters:

r_M - rate of vaporization of metal M
 a_{GM} - affinity of gas type G for metal M
 $U_{pi} I_p$ - voltage and current of any plasma which has been ignited
5 T_s - substrate temperature
 I - vaporizer-substrate distance
 P_{tot} - total gas pressure
and
 P_G - partial pressure of gas type G
10 where the latter variable is determined by
 f_G - mass flux of gas type G
 L_G - pumping capacity of the vacuum pump for gas type G
The skilled person can determine from this exper-
15 mentally the function "process composition" for each vacuum chamber and for each use. If a metal M and a gas G are involved (for example titanium and oxygen), the multidimensional parameter space described above can be reduced to a linear two-dimensional problem. For
20 example, for the titanium/oxygen system in the parameter range
 $r_{titan} = 0.1-10 \text{ mm/s}$
 $T_s = 20^\circ\text{C}-500^\circ\text{C}$
 $I = 20-120 \text{ cm}$
25 $P_{tot} = 10^{-5}-10^{-2} \text{ mbar}$
the chemical composition is a linear function of the oxygen flux f_{O_2} controlled by a flow control device. This relationship can be described by a parameterized family of curves
30 $v = 0.0245 \times (f_{O_2} + t) - 0.879$

where v describes the particle ratio of oxygen to titanium in the layer, f_{O_2} describes the oxygen flux which has been made dimensionless (oxygen flux without dimension) and t describes a family of curves parameter
35 which described the pump capacity of the chamber and geometry. In this system, the specific resistance p (without dimension) of the layer can also be described as a function of the chemical composition:

$$v = 0.357 \ln(p) - 2.1987$$

On addition of a second gas, the different affinities (a_{GM_1} , a_{GM_2}) between the metal M and the two gas types G_1 and G_2 are taken into account. The ratio of a_{GM_1} to a_{GM_2} 5 determines the parameter space in which there is a linear relation between chemical composition in the layer and the fluxes of the two gas types. On use of more than two gas types and/or more than one metal type it is possible by stochastic optimization algorithms, 10 for example genetic algorithms, to examine the parameter space experimentally in order to find parameter space regions which lead to the desired properties. In this case, the adjustment of the required ratio of amounts of the gases preferably takes place by flow 15 control devices, for example so-called mass flow controllers. It may in some cases be advantageous to ignite a plasma. Deposition of the layer on the substrate takes place in a conventional vacuum deposition apparatus familiar to the person skilled this art.

20 The layers applied to the substrate may still be chemically unstable and undergo an aging process shortly after the application and removal from the vacuum chamber. Thus, for example, titanium undergoes passivation to titanium oxide or TiO_2 , and this process 25 may take hours or even days.

The protein-, peptide- and/or saccharide-containing substance is then applied to the coated substrate. In a preferred embodiment, the substance is applied immediately or soon after the application of 30 the layer. This preferably takes place from 1 minute to 1 week, particularly preferably 1 minute to 5 hours, after the application of the layer or removal of the coated substrate from the vacuum chamber. Suitable processes for applying the substance in solution are 35 dipping and spraying. The substance is expediently applied by introducing the coated substrate into a solution containing the substance. Suitable solutions contain 1-70% by weight, preferably 1 to 40% by weight,

in particular 1 to 35% by weight, of the substance based on 100% by weight of solution. A solution containing 1-30% by weight of human albumin, in particular 1 to 15% by weight of human albumin, based on 5 100% by weight of solution, is preferably used. Besides the substance described above, the solution contains water and, where appropriate, salts, electrolytes and/or buffers. The albumin may be in the form not only of a solution for application but also of a powder 10 produced, for example, by heat shock or (salt) crystallization. In the latter case, the powder is distributed on the layer and then the article is stored in a humidity chamber. It is also possible for parts of the substance to be denatured, which extends the range of 15 applications. Thus, denatured fibrinogen may inhibit blood platelet aggregation on the surface. The substance can also be applied by bringing the coated substrate into contact with a gaseous mixture of the required substance. It is also possible to add depot 20 agents, for example anticoagulant substances or antibiotics, to the substance, which are then released continuously.

When the substance is applied by dipping in a solution, the article is stored there for from a few 25 seconds to several days at temperatures from -12 to +20°C, preferably from 0 to +7°C. The article can be marketed with the solution. In this form, it is stable for at least one month. In a preferred embodiment of the invention, the article is designed as an implant, 30 in particular as a stent.

The article according to the invention can be used for implantation, insertion or attachment in or on the animal or human body or for bringing into contact with human or animal blood or tissue or human or animal 35 cells. It is used in particular for implantation, insertion or attachment in or on the animal or human body.

The invention also relates to the use of a protein-, peptide- and/or saccharide-containing

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substance for application, in particular addition or deposition, to a layer which is defined as described above. The substance in this case is defined as described above. It is preferably selected from albumin,
5 fibrinogen and heparin, with albumin being most preferred.

Figure 1 shows diagrammatically the structure of an article which is preferred according to the invention and has the substrate (3) which is coated
10 with the PVD layer (2) and on which the substance (1) is located.

The invention is explained in detail by means of the following examples, which represent preferred embodiments of the invention.
15

Example 1:

Medical steel 1440 was mounted on a specially produced substrate holder and placed in a vacuum chamber. After evacuation of the chamber to 10^{-5} mbar,
20 the substrate was heated to 400°C. Titanium was vaporized at a rate of 0.5 nm/s using an electron gun. A nitrogen flux of 150 sccm (standard cm³) and an oxygen flux of 35 sccm were fed in using mass flow controllers. The pressure reached in the process was
25 10^{-3} mbar. A TiN_{0.95}O_{0.15} layer with a specific resistance of 1000 $\mu\Omega\text{cm}$ was applied in this way. The layer had a thickness of 1 μm .

The sample was then incubated with 1% human albumin solution (% by weight) at room temperature for
30 1 hour and subsequently dried. After the incubation with albumin, the sample was rinsed with phosphate buffer (PBS) and thus excess unbound albumin was washed off.

The sample was then cut into 5 rectangles
35 ($l \times b \times h = 76 \times 38 \times 0.2$ [mm]), of which 4 samples were incubated with filtered human plasma for 1, 2, 3 and 4 days respectively. The platelet adhesion on these 4 samples, and on the 5th sample which had been incubated only with the albumin (and not with the human

plasma), was measured. This was done by flushing citrate-anticoagulated human blood over the particular sample in a flow chamber (0.6 mm x 38 mm in size). The flow rate was 39.67 ml/min. Perfusion lasted 5 minutes
5 in each case and took place at a temperature of 37°C. After the perfusion, the particular sample was rinsed with Hepes/NaCl. Comparative samples comprised untreated substrates, that is to say medical steel of the same size and incubated and measured in the same
10 way as the sample with human plasma.

The samples and comparative samples treated in this way were then fixed and the amount of blood platelets adhering to the samples was quantified by fluorescence microscopy and stated as % of area covered
15 relative to the total area.

The results are depicted in Figure 2, where the platelet adhesion is plotted in [%] against the time in [days]. It is evident from Figure 2 that platelet adhesion to the article according to the invention is
20 reduced even after 1 day.

Example 2:

The surface of medical steel 1440 was coated in a vacuum chamber as in Example 1, but the amounts of
25 nitrogen and oxygen etc. fed in are indicated in the table below. The pressure reached in this process was 10^{-3} mbar. It was possible by altering the process parameters as specified in DE-A-195 06 188 to produce layers differing in conductivity. The layer thickness
30 was 10^{-6} m. Coated substrates with the resistances stated in the following table were obtained in this way.

No.	Specific resistance ($\mu\Omega\text{cm}$)	Composition Ti:N:O	N ₂ mass flux [sccm]	O ₂ mass flux [sccm]
1	6×10^1	1:0:0.01	-	-
2	2×10^3	1:0.8:0.2	108	44
3	6×10^3	1:0.12:1.32	35	90
4	5×10^4	1:0.01:1.88	5	140
5	2×10^5	1:0:2.05	2	120

In addition, a further 5 coated substrates were produced with the resistances depicted in Fig. 3.
5 Substance was deposited according to the invention on 5 samples, the samples being incubated in a solution containing purified human fibrinogen (grade L, KabiVitrum, 33 g of human fibrinogen/100 ml of potassium phosphate) for 30 min. The other 5 samples
10 were not treated with the substance (fibrinogen) and acted as comparative samples.

The samples and comparative samples were then investigated in a flow chamber (dimensions: $l \times b \times h = 76 \times 38 \times 0.6$ mm) for adhesion of the
15 bacterial strain *Staphylococcus epidermidis* 11047. This entailed the bacterial solution flowing over the samples and comparative samples at a flow rate of 2 ml/min for 5 hours and being quantified.

The results are depicted in Figure 3, where the total adhesion in [$\text{bacteria}/\text{cm}^2$] is plotted against the specific resistance in [$\mu\Omega\text{cm}$] of the sample. It is evident from this that the samples according to the invention show distinctly reduced adhesion.

25 Example 3:

Commercially available coronary stents were coated as described in Example 1 to result in the same specific resistance and the same layer thickness. After venting the vacuum chamber with nitrogen, the stents
30 were placed in a solution containing 5% by weight human albumin and sealed.

The stents were implanted into the coronary vessels of the hearts of 20 pigs. At the same time, untreated control stents, that is to say stents without coating and without substance, were implanted in the 5 pigs. After six weeks, the intimal hyperplasia induced by the stents and control stents was measured. To do this, samples were taken from the vessel wall immediately upstream of the implanted stents and within the implanted stents, and histological specimens were 10 prepared. The thickness of the intimal layer in the histological specimens was measured. Comparison between the stents according to the invention and the control stents showed a reduction in the intimal hyperplasia by 53% in the stents according to the invention. The 15 result was significant with $p < 0.04$.

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